

## Standard test Method for Tensile Properties of Plastics<sup>1</sup>

This standard is issued under the fixed designation D 638; the number immediately following the designation indicates the year of original adoption or, in the case of revision, the year of last revision. A number in parentheses indicates the year of last reapproval. A superscript epsilon ( $\epsilon$ ) indicates an editorial change since the last revision or reapproval.

This test method has been approved for use by agencies of the Department of Defense.

Consult the DoD Index of Specifications and Standards for the specific year of issue which has been adopted by the Department of Defense.

### 1. Scope

- 1.1 This test method covers the determination of the tensile properties of unreinforced and reinforced plastics in the form of standard dumbbell-shaped test specimens when tested under defined conditions of pretreatment, temperature, humidity, and testing machine speed.

Note 1—This test method and ISO 527-1 are technically equivalent.

Note 2—A complete metric companion to Test Method D 638 has been developed—D638M.

Note 3—This test method is not intended to cover precise physical procedures. It is recognized that the constant-rate-of-cross-head-movement type of test leaves much to be desired from a theoretical standpoint, that wide differences may exist between rate of crosshead movement and rate of strain between gage marks on the specimen, and that the testing speeds specifies disguise important effects characteristic of materials in the plastic state. Further, it is realized that variations in the thicknesses of test specimens, which are permitted by these procedures, produce variations in the surface-volume ratios of such specimens, and that these variations may influence the test results. Hence, where directly comparable results are desired, all samples should be of equal thickness. Special additional tests should be used where more precise physical data are needed.

Note 4—This test method may be used for testing phenolic molded resin or laminated materials.

However, where these materials are used as electrical insulation, such materials should be tested in accordance with Test Methods D 229 and Test Method D 651.

Note 5—For tensile properties of resin-matrix composites reinforced with oriented continuous or discontinuous high modulus  $>20$  GPa ( $>3.0 \times 10^6$  psi) fibers, tests shall be made in accordance with Test Method D 3039.

- 1.2 This test method can be used for testing materials of any thickness up to 14 mm (0.55 in.).

However, for testing specimens in the form of thin sheeting, including film less than 1.0 mm (0.04 in.) in thickness, Test Methods D882 is the preferred test method. Material with a thickness greater than 14 mm (0.55 in.) must be reduced by machining.

- 1.3 The values stated in SI units are to be regarded as the standard. The values given in parentheses are for information only.

- 1.4 This standard does not purport to address all of the safety concerns, if any, associated with its use. It is the responsibility of the user of this standard to establish appropriate safety and health practices and determine the applicability of regulatory limitations prior to use.

### 2. Referenced Documents

- 2.1 ASTM Standards:

D229 Test Methods for Rigid Sheet and Plate Materials Used for Electrical Insulation<sup>2</sup>.

D374 Test Methods for Thickness of Solid Electrical Insulation<sup>2</sup>.

D412 Test Methods for Vulcanized Rubber and Thermoplastic Rubbers and Elastomers—Tension<sup>3</sup>.

D618 Practice for Conditioning Plastics and Electrical Insulating Materials for Testing<sup>4</sup>.

D638M Test Method for Tensile Properties of Plastics (Metric)<sup>4</sup>.

D651 Test Method for Tensile Strength of Molded Electrical Insulating Materials<sup>2</sup>.

D882 Test Methods for Tensile Properties of Thin Plastic Sheeting<sup>4</sup>.

D883 Terminology Relating to Plastics<sup>4</sup>.

D1822 Test Method for Tensile Properties of Fiber-Resin Composites<sup>5</sup>.

D3039 Classification System for Specifying Plastic Materials<sup>6</sup>.

D4066 Specification for Nylon Injection and Extrusion Materials (PA)<sup>6</sup>.

E 4 Practices for Force Verification of Testing Machines<sup>7</sup>.

E 83 Practice for Verification and Classification of Extensometers<sup>7</sup>.

E 691 Practice for Conducting an Interlaboratory Study to Determine the Precision of a Test

Method<sup>8</sup>.

- 2.2 ISO Standard:  
ISO 527 – 1 Determination of Tensile Properties.

### 3. Terminology

- 3.1 Definitions—Definitions of terms applying to this test method appear in Terminology D 883 and Annex A2.

### 4. Significance and Use

- 4.1 This test method is designed to produce tensile property data for the control and specification of plastic materials. These data are also useful for qualitative characterization and for research and development. For many materials, there may be a specification that requires the use of this test method, but with some procedural modifications that take precedence when adhering to the specification. Therefore, it is advisable to refer to that material specification before using this test method. Table 1 in Classification D 4000 lists the ASTM materials standards that currently exist.
- 4.2 Tensile properties may vary with specimen preparation and with speed and environment of testing. Consequently, where precise comparative results are desired, these factors must be carefully controlled.
- 4.2.1 It is realized that a material cannot be tested without also testing the method of preparation of that material. Hence, when comparative tests of materials per se are desired, the greatest care must be exercised to ensure that all samples are prepared in exactly the same way, unless the test is to include the effects of sample preparation. Similarly, for referee purposes or comparisons within any given series of specimens, care must be taken to secure the maximum degree of uniformity in details of preparation, treatment, and handling.
- 4.3 Tensile properties may provide useful data for plastics engineering design purposes. However, because of the high degree of sensitivity exhibited by many plastics to rate of straining and environmental conditions, data obtained by this test method cannot be considered valid for applications involving load-time scales or environments widely different from those of this test method. In cases of such dissimilarity, no reliable estimation of the limit of usefulness can be made for most plastics. This sensitivity to rate of straining and environment necessitates testing over a broad load-time scale (including impact and creep) and range of environmental conditions if tensile properties are to suffice for engineering design purposes.

Note 6—Since the existence of a true elastic limit in plastics (as in many other organic materials and in many metals) is debatable, the propriety of applying the term “elastic modulus” in its quoted, generally accepted definition to describe the “stiffness” or “rigidity” of a plastic has been seriously questioned. The exact stress-strain characteristics of plastic materials are highly dependent on such factors as rate of application of stress, temperature, previous history of specimen, etc. However, stress-strain curves for plastics, determined as described in this test method, almost always show a linear region at low stresses, and a straight line drawn tangent to this portion of the curve permits calculation of an elastic modulus of the usually defined type. Such a constant is useful if its arbitrary nature and dependence on time, temperature, and similar factors are realized.

### 5. Apparatus

- 5.1 Testing Machine—A testing machine of the constant-rate-of-crosshead-movement type and comprising essentially the following:
- 5.1.1 Fixed Member—A fixed or essentially stationary member carrying one grip.
- 5.1.2 Movable Member—A movable member carrying a second grip.
- 5.1.3 Grips—Grips of holding the test specimen between the fixed member and the movable member of the testing machine can be either the fixed or self-aligning type.
- 5.1.3.1 Fixed grips are rigidly attached to the fixed and movable member of the testing machine. When this type of grip is used extreme care should be taken to ensure that the test specimen is inserted and clamped so that the long axis of the test specimen coincides with the direction of pull through the center line of the grip assembly.
- 5.1.3.2 Self-aligning grips are attached to the fixed and movable members of the testing machine in such a manner that they will move freely into alignment as soon as any load is applied so that the long axis of the test specimen will coincide with the direction of the applied pull through the center line of the grip assembly. The

specimens should be aligned as perfectly as possible with the direction of pull so that no rotary motion that may induce slippage will occur in the grips; there is a limit to the amount of misalignment self-aligning grips will accommodate.

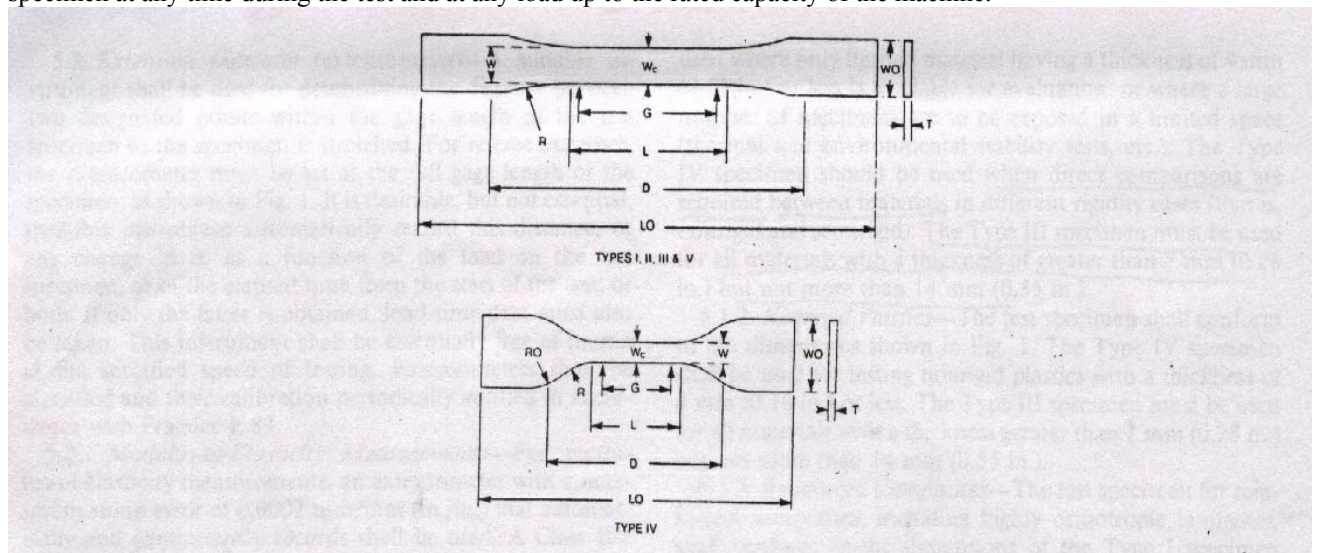
5.1.3.3 The test specimen shall be held in such a way that slippage relative to the grips is prevented insofar as possible. Grip surfaces that are deeply scored or serrated with a pattern similar to those of a coarse single-cut file, serrations about 2.4mm (0.09 in.) apart and about 1.6 mm (0.06 in.) deep, have been found satisfactory for most thermoplastics. Finer serrations have been found to be more satisfactory for harder plastics, such as the thermosetting materials. The serrations should be kept clean and sharp. Breaking in the grips may occur at times, even when deep serrations or abraded specimen surfaces are used; other techniques must be used in these cases. Other techniques that have been found useful, particularly with smooth-faced grips, are abrading that portion of the surface of the specimen that will be in the grips, and interposing thin pieces of abrasive cloth, abrasive paper, or plastic or rubber-coated fabric, commonly called hospital sheeting, between the specimen and the grip surface. No. 80 double-sided abrasive paper has been found effective in many cases. An open-mesh fabric, in which the threads are coated with abrasive paper has been effective. Reducing the cross-sectional area of the specimen may also be effective. The use of special types of grips is sometimes necessary to eliminate slippage and breakage in the grips.

5.1.4 Drive Mechanism—A drive mechanism for imparting to the movable member a uniform, controlled velocity with respect to the stationary member, with this velocity to be regulated as specified in Section 9.

5.1.5 Load Indicator—A suitable load-indicating mechanism capable of showing the total tensile load carried by the test specimen when held by the grips. This mechanism shall be essentially free of inertia lag at the specified rate of testing and shall indicate the load with an accuracy of  $\pm 1\%$  of the indicated value, or better. The accuracy of the testing machine shall be verified in accordance with Practices E 4.

Note 7—Experience has shown that many testing machines now in use are incapable of maintaining accuracy for as long as the periods between inspection recommended in Practices E 4. Hence, it is recommended that each machine be studied individually and verified as often as may be found necessary. It frequently will be necessary to perform this function daily.

5.1.6 The fixed member, movable member, drive mechanism, and grips shall be constructed of such materials and in such proportions that the total elastic longitudinal strain of the system constituted by these parts does not exceed 1% of the total longitudinal strain between the two gage marks on the test specimen at any time during the test and at any load up to the rated capacity of the machine.



Specimen Dimensions for Thickness,  $T$ , mm (in.)<sup>D</sup>

Dimensions (see drawings)	7 (0.28) or under		Over 7 to 14 (0.28 to 0.55) incl.	4 (0.16) or under		Tolerances
	Type I	Type II	Type III	Type IV <sup>g</sup>	Type V <sup>h</sup>	
$W$ —Width of narrow section <sup>A, B</sup>	13 (0.50)	6 (0.25)	19 (0.75)	6 (0.25)	3.18 (0.125)	$\pm 0.5$ ( $\pm 0.02$ ) <sup>g, i</sup>
$L$ —Length of narrow section	57 (2.25)	57 (2.25)	57 (2.25)	33 (1.30)	9.53 (0.375)	$\pm 0.5$ ( $\pm 0.02$ ) <sup>i</sup>
$W_0$ —Width over-all, min <sup>E</sup>	19 (0.75)	19 (0.75)	29 (1.13)	19 (0.75)	...	+6.4 (+0.25)
$W_0$ —Width over-all, min <sup>E</sup>	...	...	...	...	9.53 (0.375)	+3.18 (+0.125)
$L_0$ —Length over-all, min <sup>F</sup>	165 (6.5)	183 (7.2)	246 (9.7)	115 (4.5)	63.5 (2.5)	no max (no max)
$G$ —Gage length <sup>C</sup>	50 (2.00)	50 (2.00)	50 (2.00)	...	7.62 (0.300)	+0.25 ( $\pm 0.010$ ) <sup>i</sup>
$G$ —Gage length <sup>C</sup>	...	...	...	25 (1.00)	...	+0.13 ( $\pm 0.005$ )
$D$ —Distance between grips	115 (4.5)	135 (5.3)	115 (4.5)	65 (2.5) <sup>h</sup>	25.4 (1.0)	$\pm 5$ ( $\pm 0.2$ )
$R$ —Radius of fillet	76 (3.00)	76 (3.00)	76 (3.00)	14 (0.56)	12.7 (0.5)	$\pm 1$ ( $\pm 0.04$ ) <sup>i</sup>
$RO$ —Outer radius (Type IV)	...	...	...	25 (1.00)	...	$\pm 1$ ( $\pm 0.04$ )

<sup>A</sup> The width at the center  $W_0$  shall be  $+0.00$  mm,  $-0.10$  mm ( $+0.000$  in.,  $-0.004$  in.) compared with width  $W$  at other parts of the reduced section. Any reduction in  $W$  at the center shall be gradual, equally on each side so that no abrupt changes in dimension result.

<sup>B</sup> For molded specimens, a draft of not over 0.13 mm (0.005 in.) may be allowed for either Type I or II specimens 3.2 mm (0.13 in.) in thickness, and this should be taken into account when calculating width of the specimen. Thus a typical section of a molded Type I specimen, having the maximum allowable draft, could be as follows:

<sup>C</sup> Test marks or initial extensometer span.

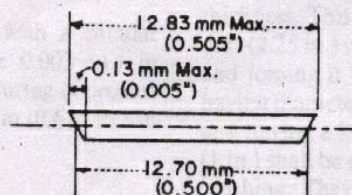
<sup>D</sup> Thickness,  $T$ , shall be  $3.2 \pm 0.4$  mm ( $0.13 \pm 0.02$  in.) for all types of molded specimens, and for other Types I and II specimens where possible. If specimens are machined from sheets or plates, thickness,  $T$ , may be the thickness of the sheet or plate provided this does not exceed the range stated for the intended specimen type. For sheets of nominal thickness greater than 14 mm (0.55 in.) the specimens shall be machined to  $14 \pm 0.4$  mm ( $0.55 \pm 0.02$  in.) in thickness, for use with the Type III specimen. For sheets of nominal thickness between 14 and 51 mm (0.55 and 2 in.) approximately equal amounts shall be machined from each surface. For thicker sheets both surfaces of the specimen shall be machined and the location of the specimen with reference to the original thickness of the sheet, shall be noted. Tolerances on thickness less than 14 mm (0.55 in.) shall be those standard for the grade of material tested.

<sup>E</sup> Overall widths greater than the minimum indicated may be desirable for some materials in order to avoid breaking in the grips.

<sup>F</sup> Overall lengths greater than the minimum indicated may be desirable either to avoid breaking in the grips or to satisfy special test requirements.

<sup>G</sup> For the Type IV specimen, the internal width of the narrow section of the die shall be  $6.00 \pm 0.05$  mm ( $0.250 \pm 0.002$  in.). The dimensions are essentially those of Die C in Test Methods D 412.

<sup>H</sup> When self-tightening grips are used, for highly extensible polymers, the distance between grips will depend upon the types of grips used and may not be critical if maintained uniform once chosen.



<sup>I</sup> The Type V specimen shall be machined or die cut to the dimensions shown, or molded in a mold whose cavity has these dimensions. The dimensions shall be:

- $W = 3.18 \pm 0.03$  mm ( $0.125 \pm 0.001$  in.),
- $L = 9.53 \pm 0.08$  mm ( $0.375 \pm 0.003$  in.),
- $G = 7.62 \pm 0.02$  mm ( $0.300 \pm 0.001$  in.), and
- $R = 12.7 \pm 0.08$  mm ( $0.500 \pm 0.003$  in.).

The other tolerances are those in the table.

<sup>J</sup> Supporting data on the introduction of the L specimen of Test Method D 1822 as the Type V specimen are available from ASTM Headquarters. Request RR.D 20-1038.

FIG. 1 Tension Test Specimens for Sheet, Plate, and Molded Plastics

5.2 Extension Indicator (extensometer)—A suitable instrument shall be used for determining the distance between two designated points within the gage length of the test specimen as the specimen is stretched. For referee purposes, the extensometer must be set at the full gage length of the specimen, as shown in Fig. 1. It is desirable, but not essential, that this instrument automatically record this distance, or any change in it, as a function of the load on the test specimen, or of the elapsed time from the start of the test, or both. If only the latter is obtained, load-time data must also be taken. This instrument shall be essentially free of inertia at the specified speed of testing. Extensometers shall be classified and their calibration periodically verified in accordance with Practice E83.

5.2.1 Modulus-of Elasticity Measurements—For modulus-of-elasticity measurements, an extensometer with a maximum strain error of 0.0002 mm/mm (in./in.) that automatically and continuously records shall be used. A class B-2 extensometer (Practice E 83) meets this requirement.

5.2.2 Low-Extension Measurements—For elongation-at-yield and low-extension measurements (nominally 20% or less), the same above extensometer, attenuated to 20% extension, may be used. In any case, the extensometer system must meet at least Class C (Practice E 83) requirements, which include a fixed strain error of 0.001 strain or  $\pm 1.0\%$  of the indicated strain, whichever is greater.

- 5.2.3 High-Extension Measurements—For measurement at elongations greater than 20%, measuring techniques with error no greater than  $\pm 10\%$  of the measured value are acceptable.
- 5.3 Micrometers—Suitable micrometers for measuring the width and thickness of the test specimen to an incremental discrimination of at least 0.025 mm (0.001 in.) should be used. All width and thickness measurements of rigid and semirigid plastics may be measured with a hand micrometer with ratchet. A suitable instrument for measuring the thickness of nonrigid test specimens shall have: (1) a contact measuring pressure of  $25 \pm 2.5$  kPa ( $3.6 \pm 0.36$  psi), (2) a movable circular contact foot  $6.35 \pm 0.025$  mm ( $0.250 \pm 0.001$  in.) in diameter, and (3) a lower fixed anvil large enough to extend beyond the contact foot in all directions and being parallel to the contact foot within 0.005 mm (0.0002 in.) over the entire foot area. Flatness of foot and anvil shall conform to the portion of the Calibration Section of Test Methods D374, which addresses “flatness of surfaces of micrometers.”
- 5.3.1 An optional instrument equipment with a circular contact foot  $15.88 \pm 0.08$  ( $0.625 \pm 0.003$  in.) in diameter is recommended for thickness measuring of process samples or larger specimens at least 15.88 mm (0.625 in.) in minimum width.

## 6. Test Specimens

### 6.1 Sheet, Plate, and Molded Plastics:

- 6.1.1 Rigid and Semirigid Plastics—The test specimen shall conform to the dimensions shown in Fig. 1. The Type I specimen is the preferred specimen and shall be used where sufficient material having a thickness of 7 mm (0.28 in.) or less is available. The Type II specimen may be used when a material does not break in the narrow section with the preferred Type I specimen. The Type V specimen shall be used where only limited material having a thickness of 4 mm (0.16 in.) or less is available for evaluation, or where a large number of specimens are to be exposed in a limited space (thermal and environmental stability tests, etc.). the Type IV specimen should be used when direct comparisons are required between materials in different rigidity cases (that is, nonrigid and semirigid). The Type III specimen must be used for all materials with a thickness of greater than 7 mm (0.28 in.) but not more than 14 mm (0.55 in.).
- 6.1.2 Nonrigid Plastics—The test specimen shall conform to the dimensions shown in Fig. 1. The Type IV specimen shall be used for testing nonrigid plastics with a thickness of 4 mm (0.16 in.) or less. The Type III specimen must be used for all materials with a thickness greater than 7 mm (0.28 in.) but not more than 14 mm (0.55 in.).
- 6.1.3 Reinforced Composites—The test specimen for reinforced composites, including highly orthotropic laminates, shall conform to the dimensions of the Type I specimen shown in Fig. 1.
- 6.1.4 Preparation—Test specimens shall be prepared by machining operations, or die cutting, from materials in sheet, plate, slab, or similar form. Materials thicker than 14 mm (0.55 in.) must be machined to 14 mm (0.55 in.) for used as Type III specimens. Specimens can also be prepared by molding the material to be tested.

Note 8—Test results have shown that for some materials such as glass cloth, SMC, and BMC laminates, other specimen types should be considered to ensure breakage within the gage length of the specimen, as mandated by 8.3.

Note 9—When preparing specimens from certain composite laminates such as woven roving, or glass cloth, care must be exercised in cutting the specimens parallel to the reinforcement. The reinforcement will be significantly weakened by cutting on a bias, resulting in lower laminate properties, unless testing of specimens in a direction other than parallel with the reinforcement constitutes a variable being studied.

Note 10—Specimens prepared by injection molding may have different tensile properties than specimens prepared by machining or die-cutting because of the orientation induced. This effect may be more pronounced in specimens with narrow sections.

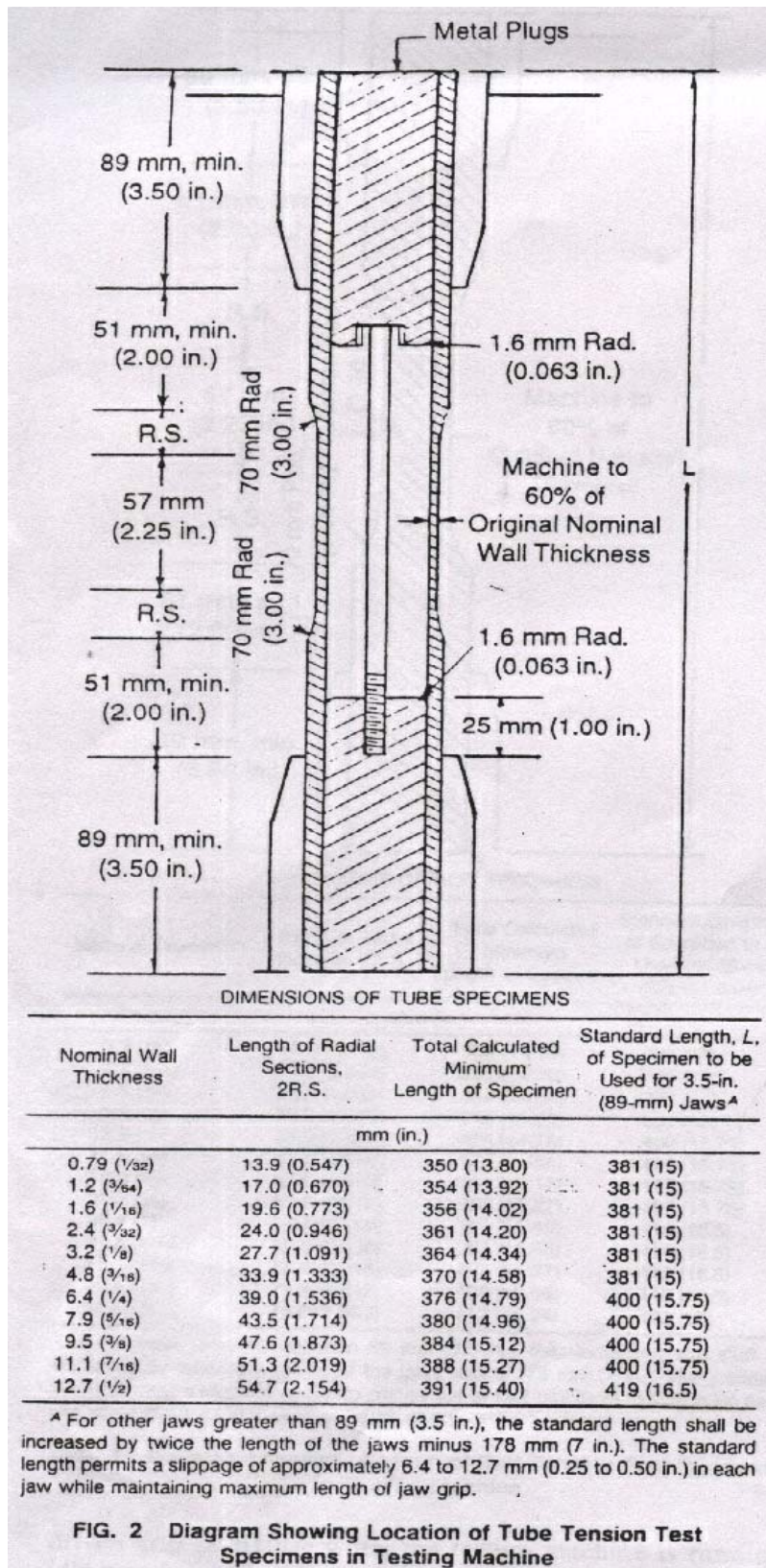
### 6.2 Rigid Tubes:

- 6.2.1 The test specimen for rigid tubes shall be as shown in Fig. 2. The length,  $L$ , shall be as shown in the table in Fig. 2. A groove shall be machined around the outside of the specimen at the center of its length so that the wall section after machining shall be 60% of the original nominal wall thickness. This groove shall consist of a straight section 57.2 mm (2.25 in.) in length with a radius of 76 mm (3 in.) at each end joining it to the outside diameter. Steel or brass plugs having diameters such that they will fit snugly inside the tube and having a length equal to the full jaw length plus 25 mm (1 in.) shall be placed in the ends of the specimens to prevent crushing. They can be located conveniently in the

tube by separating and supporting them on a threaded metal rod. Details of plugs and test assembly are shown in Fig. 2.

6.3 Rigid Rods:

- 6.3.1 The test specimen for rigid rods shall be as shown in Fig. 3. The length, L, shall be as shown in the table in Fig. 3. A groove shall be machined around the specimen at the center of its length so that the diameter of the machined portion shall be 60% of the original nominal diameter. This groove shall consist of a straight section 57.2 mm (2.25 in.) in length with a radius of 76 mm (3 in.) at each end joining it to the outside diameter.



- 6.4 All surfaces of the specimen shall be free of visible flaws, scratches, or imperfections. Marks left by coarse machining operations shall be carefully removed with a fine file or abrasive, and the field surfaces shall then be smoothed with abrasive paper (No. 00 or finer). The finishing sanding strokes shall be made in a direction parallel to the long axis of the test specimen. All flash shall be removed from a molded specimen, taking great care not to disturb the molded surfaces. In machining a specimen, undercuts that would exceed the dimensional tolerances shown in Fig. 1 shall be scrupulously avoided. Care shall also be taken to avoid other common

machining errors.

- 6.5 If it is necessary to place gage marks on the specimen, this shall be done with a wax crayon or India ink that will not affect the material being tested. Gage marks shall not be scratched, punched, or impressed on the specimen.
- 6.6 When testing materials that are suspected of anisotropy, duplicate sets of test specimens shall be prepared, having their long axes respectively parallel with, and normal to, the suspected direction of anisotropy.

## **7. Conditioning**

- 7.1 Conditioning—Condition the test specimens at  $23 \pm 2^{\circ}\text{C}$  ( $73.4 \pm 3.6^{\circ}\text{F}$ ) and  $50 \pm 5\%$  relative humidity for not less than 40 h prior to test in accordance with Procedure A of Practice D618, for those tests where conditioning is required. In cases of disagreement, the tolerances shall be  $\pm(\pm 1^{\circ}\text{C}) 1.8^{\circ}\text{F}$  and  $\pm 2\%$  relative humidity.
  - 7.1.1 Note that for some hygroscopic material, such as nylons, the material specifications (for example, Specification D 4066) call for testing “dry as-molded specimens.” Such requirements take precedence over the above routine preconditioning to 50% relative humidity and require sealing the specimens in water vapor-impermeable containers as soon as molded and not removing them until ready for testing.
- 7.2 Test Conditions—Conduct tests in the Standard Laboratory Atmosphere of  $(23 \pm 2^{\circ}\text{C}) 73.4 \pm 3.6^{\circ}\text{F}$  and  $50 \pm 5\%$  relative humidity, unless otherwise specified in the test methods. In cases of disagreement, the tolerances shall be  $\pm(1^{\circ}\text{C}) 1.8^{\circ}\text{F}$  and  $\pm 2\%$  relative humidity.

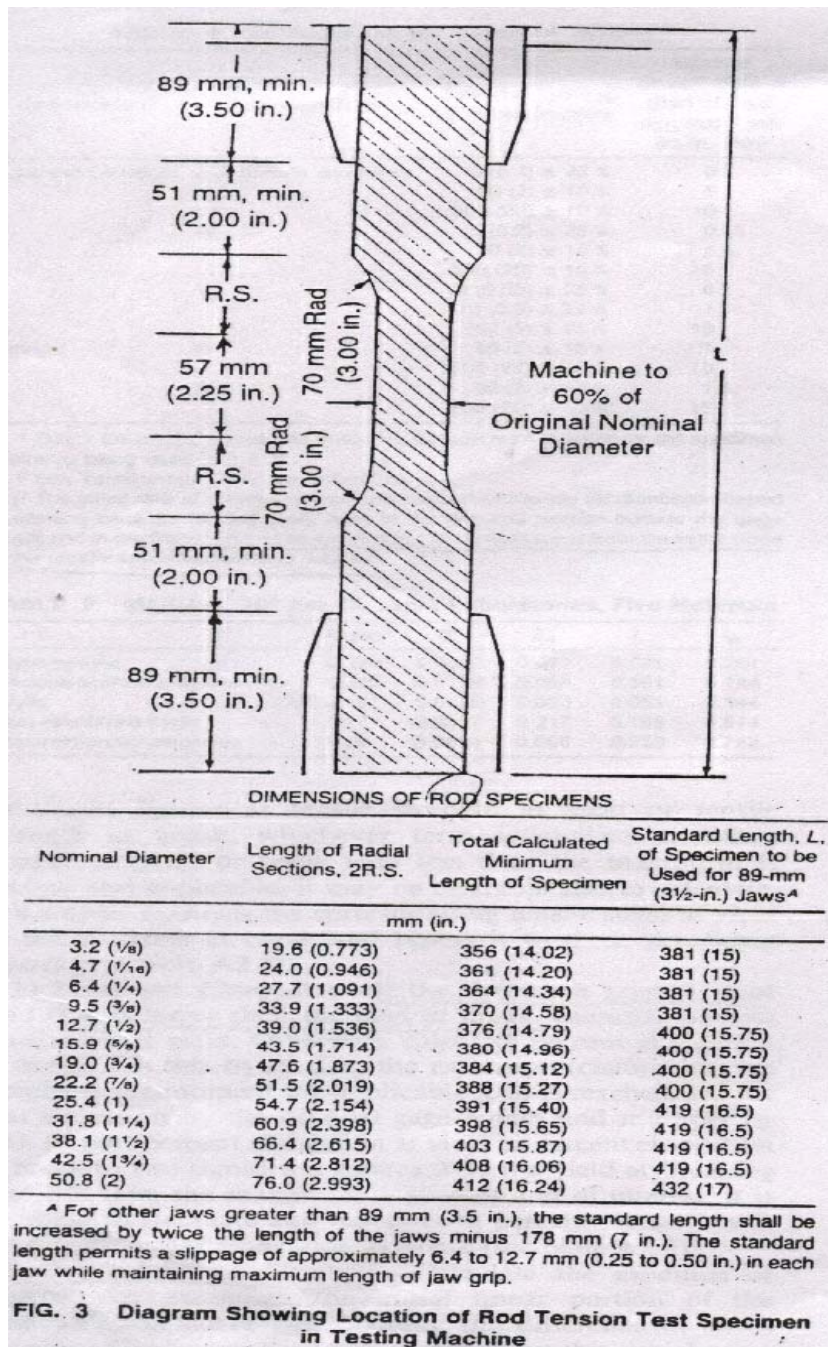
## **8. Number of Test Specimens**

- 8.1 Test at least five specimens for each sample in the case of isotropic materials.
- 8.2 Test ten specimens, five normal to, and five parallel with, the principle axis of anisotropy, for each sample in the case of anisotropic materials.
- 8.3 Discard specimens that break at some obvious fortuitous flaw, or that do not break between the predetermined gage marks, and make retests, unless such flaws constitute a variable to be studied.

Note 12—Before testing, all transparent specimens should be inspected in a polariscope. Those which show atypical or concentrated strain patterns should be rejected, unless the effects of these residual strains constitute a variable to be studied.

## **9. Speed of Testing**

- 9.1 Speed of testing shall be the relative rate of motion of the grips or test fixtures during the test. Rate of motion of the driven grip or fixture when the testing machine is running idle may be used, if it can be shown that the resulting speed of testing is within the limits of variation allowed.



- 9.2 Choose the speed of testing from Table 1. Determine this chosen speed of testing by the specification for the material being tested, or by agreement between those speed shown in Table 1 for the specimen geometry being used, which gives rupture within 1/2 to 5 min testing time.
- 9.3 Modulus determinations may be made at the speed selected for the other tensile properties when the recorder response and resolution are adequate.

## 10. Procedure

- 10.1 Measure the width and thickness of rigid flat specimens (Fig. 1) with a suitable micrometer to the nearest 0.025 mm (0.001 in.) at several points along their narrow sections. Measure the thickness of nonrigid specimens (produced by a Type IV die) in the same manner with the required dial micrometer. Take the width of this specimen as the distance between the cutting edges of the die in the narrow section. Measure the diameter of rod specimens, to the nearest 0.025 mm (0.001 in.) at a minimum of two points 90° apart; make these measurements along the groove for specimens so constructed. Use plugs in testing tube specimens, as shown in Fig. 2.
- 10.2 Place the specimen in the grips of the testing machine, taking care to align the long axis of the specimen and the grips with an imaginary line joining the points of attachment of the grips to the

machine. The distance-between the ends of the gripping surfaces, when using flat specimens, shall be as indicated in Fig. 1. On tube and rod specimens, the location for the grips shall be as shown in Fig. 2 and 3. Tighten the grips evenly and firmly to the degree necessary to prevent slippage of the specimen during the test, but not to the point where the specimen would be crushed.

10.3 Attach the extension indicator. When modulus is being determined, the extension indicator must continuously record the distance the specimen is stretched (elongated) within the gage length as a function of the load through the initial (linear) portion of the load-elongation curve.

Note 13—Modulus of materials is determined from the slope of the linear portion of the stress-strain curve. For most plastics, this linear portion is very small, occurs very rapidly, and must be recorded automatically. The change in jaw separation is never to be used for calculating modulus or elongation.

10.4 Set the speed of testing at the proper rate as required in Section 9, and start the machine.

10.5 Record the load-extension curve of the specimen.

10.6 Record the load and extension at the yield point (if one exists) and the load and extension at the moment of rupture.

Note 14—If it is desired to measure both modulus and failure properties (yield or break, or both), it may be necessary, in the case of highly extensible material, to run two independent tests. The high magnification extensometer normally used to determine properties up to the yield point may not be suitable for tests involving high extensibility. If allowed to remain attached to the specimen, the extensometer could be permanently damaged. A broad range incremental extensometer or hand rule technique may be needed when such material are taken to rupture.

## 11. Calculation

11.1 Tensile Strength—Calculate the tensile strength by dividing the maximum load in newtons (or pounds-force) by the original minimum cross-sectional area of the specimen in square metres (or square inches). Express the result in pascals (or pounds-force per square inch) and report it to three significant figures as tensile strength at yield or tensile strength at break, whichever term is applicable. When a nominal yield or break load less than the maximum is present and applicable, it may be desirable also to calculate, in a similar manner, the corresponding tensile stress at yield or tensile stress at break and report it to three significant figures (see Note A2.8).

**TABLE 1 Designations for Speed of Testing<sup>A</sup>**

Classification <sup>B</sup>	Specimen Type	Speed of Testing, mm/min (n./min)	Nominal Strain <sup>C</sup> Rate at Start of Test, mm/mm•min (in./in. •min)
Rigid and Semirigid	I, II, III rods and tubes	5(0.2) ±25%	0.1
		50(2) ±10%	1
		500(20) ±10%	10
	IV	5(0.2) ±25%	0.15
		50(2) ±10%	1.5
		500(20) ±10%	15
	V	1(0.05) ±25%	0.1
		10(0.5) ±25%	1
		100(5) ±25%	10
	Nonrigid	III	50(2) ±10%
500(20) ±10%			10
IV		50(2) ±10%	1.5
		500(20) ±10%	15

<sup>A</sup> Select the lowest speed that produces rupture in 1/2 to 5 min for the specimen geometry being used (see 9.2).

<sup>B</sup> See Terminology D883 for definitions.

<sup>C</sup> The initial rate of straining cannot be calculated exactly for dumbbell-shaped specimens because of extension, both in the reduced section outside the gage length and in the fillets. This initial strain rate can be measured from the initial slope of the tensile strain-versus-time diagram.

**TABLE 2 Modulus, 10<sup>6</sup> psi, for Eight Laboratories, Five Materials**

	Mean	S <sub>r</sub>	S <sub>R</sub>	I <sub>r</sub>	I <sub>R</sub>
Polypropylene	0.210	0.0089	0.071	0.025	0.201
Cellulose acetate butyrate	0.246	0.0179	0.035	0.051	0.144
Acrylic	0.481	0.0179	0.063	0.051	0.144
Glass-reinforced nylon	1.17	0.0537	0.217	0.152	0.614
Glass-reinforced polyester	1.39	0.0894	0.266	0.253	0.753

11.2 Percent Elongation—If the specimen gives a yield load that is larger than the load at break, calculate percent elongation at yield. Otherwise, calculate percent elongation at break. Do this by reading the extension (change in gage length) at the moment the applicable load is reached. Divide that extension by the original gage length and multiply by 100. Report percent elongation at yield or percent elongation at break to two significant figures. When a yield or breaking load less than the maximum is present and of interest, it is desirable to calculate and report both percent elongation at yield and percent elongation at break (see Note A2.2).

11.3 Modulus of Elasticity—Calculate the modulus of elasticity by extending the initial linear portion of the load-extension curve and dividing the difference in stress corresponding to any segment of section on this straight line by the corresponding difference in strain. All elastic modulus values shall be computed using the average initial cross-sectional area of the test specimens in the calculations. The result shall be expressed in pascals (pounds-force per square inch) and reported to three significant figures.

11.4 Secant modulus—At a designated strain, this shall be calculated by dividing the corresponding stress (nominal) by the designated strain. Elastic modulus values are preferable and shall be calculated whenever possible. However, for materials where no proportionality is evident, the secant values shall be calculated. Draw the tangent as directed in A1.3 and Fig. A1.2, and mark off the designated strain from the yield point where the tangent line goes through zero stress. The stress to be used in the calculation is then determined by dividing the load-extension curve by the original average cross-sectional area of the specimen.

**TABLE 3 Tensile Stress at Yield, 10<sup>3</sup> psi, for Eight Laboratories, Three Materials**

	Mean	S <sub>r</sub>	S <sub>R</sub>	I <sub>r</sub>	I <sub>R</sub>
Polypropylene	3.63	0.022	0.161	0.062	0.456
Cellulose acetate butyrate	5.01	0.058	0.227	0.164	0.642
Acrylic	10.4	0.067	0.317	0.190	0.897

**TABLE 4 Elongation at Yield, %, for Eight Laboratories, Three Materials**

	Mean	S <sub>r</sub>	S <sub>R</sub>	I <sub>r</sub>	I <sub>R</sub>
Cellulose acetate butyrate	3.65	0.27	0.62	0.76	1.75
Acrylic	4.89	0.21	0.55	0.59	1.56
Polypropylene	8.79	0.45	5.86	1.27	16.5

11.5 For each series of tests, calculate the arithmetic mean of all values obtained and report it as the “average value” for the particular property in question.

11.6 Calculate the standard deviation (estimated) as follows and report it to two significant figures:

$$s = \sqrt{(\sum X^2 - n\bar{X}^2)/(n-1)}$$

where:

s = estimated standard deviation,

X = value of single observation,

n = number of observations, and

$\bar{X}$  = arithmetic mean of the set of observations

11.7 See Annex A1 for information on toe compensation.

## 12. Report

12.1 Report the following information:

12.1.1 Complete identification of the material tested, including type, source, manufacturer’s code numbers, form, principal dimensions, previous history, etc.,

12.1.2 Method of preparing test specimens,

12.1.3 Type of test specimen and dimensions,

- 12.1.4 Conditioning procedure used,
  - 12.1.5 Atmospheric conditions in test room,
  - 12.1.6 Number of specimens tested,
  - 12.1.7 Speed of testing,
  - 12.1.8 Tensile strength at yield or break, average value, and standard deviation,
  - 12.1.9 Tensile stress at yield or break, if applicable, average value, and standard deviation,
  - 12.1.10 Percent elongation at yield or break (or both, as applicable), average value, and standard deviation,
  - 12.1.11 Modulus of elasticity, average value, and standard deviation, and
  - 12.1.12 Date of test.
13. Precision and Bias<sup>10</sup>
- 13.1 Table 2 through 6 are based on a round robin test conducted in 1984, involving five materials tested by eight laboratories using the Type I specimen, all of nominal 0.125-in. thickness. Each test result was based on five individual determinations. Each laboratory obtained two test results for each material.

**TABLE 5 Tensile Strength at Break, 10<sup>3</sup> psi, for Eight Laboratories, Five Materials<sup>A</sup>**

	Mean	S <sub>r</sub>	S <sub>R</sub>	I <sub>r</sub>	I <sub>R</sub>
Polypropylene	2.97	1.54	1.65	4.37	4.66
Cellulose acetate butyrate	4.82	0.058	0.180	0.164	0.509
Acrylic	9.09	0.452	0.751	1.27	2.13
Glass-reinforced polyester	20.8	0.233	0.437	0.659	1.24
Glass-reinforced nylon	23.6	0.277	0.698	0.784	1.98

<sup>A</sup> Tensile strength and elongation at break values obtained for unreinforced propylene plastics generally are highly variable due to inconsistencies in necking or “drawing” of the center section of the test bar. Since tensile strength and elongation at yield are more reproducible and relate in most cases to the practical usefulness of a molded part, they are generally recommended for specification purposes.

**TABLE 6 Elongation at Break, %, for Eight Laboratories, Five Materials<sup>A</sup>**

	Mean	S <sub>r</sub>	S <sub>R</sub>	I <sub>r</sub>	I <sub>R</sub>
Glass-reinforced polyester	3.68	0.20	2.33	0.570	6.59
Glass-reinforced nylon	3.87	0.10	2.13	0.283	6.03
Acrylic	13.2	2.05	3.65	5.80	10.3
Cellulose acetate butyrate	14.1	1.87	6.62	5.29	18.7
Polypropylene	293.0	50.9	119.0	144.0	337.0

<sup>A</sup> Tensile strength and elongation at break values obtained for unreinforced propylene plastics generally are highly variable due to inconsistencies in necking or “drawing” of the center section of the test bar. Since tensile strength and elongation at yield are more reproducible and relate in most cases to the practical usefulness of a molded part, they are generally recommended for specification purposes.

**TABLE 7 Tensile Yield Strength, for Ten Laboratories, Eight Materials**

Material	Test Speed, in./min	Values Expressed in psi Units				
		Average	S <sub>r</sub>	S <sub>R</sub>	I <sub>r</sub>	I <sub>R</sub>
LDPE	20	1544	52.4	64.0	146.6	179.3
LDPE	20	1894	53.1	61.2	148.7	171.3
LLDPE	20	1879	74.2	99.9	207.8	279.7
LLDPE	20	1791	49.2	75.8	137.9	212.3
LLDPE	20	2900	55.5	87.9	155.4	246.1
LLDPE	20	1730	63.9	96.0	178.9	268.7
HDPE	2	4101	196.1	371.9	549.1	1041.3
HDPE	2	3523	175.9	478.0	492.4	1338.5

**TABLE 8 Tensile Yield Elongation, for Eight Laboratories, Eight Materials**

Material	Test Speed, in./min	Values Expressed in Percent Units				
		Average	S <sub>r</sub>	S <sub>R</sub>	I <sub>r</sub>	I <sub>R</sub>
LDPE	20	17.0	1.26	3.16	3.52	8.84
LDPE	20	14.6	1.02	2.38	2.86	6.67
LLDPE	20	15.7	1.37	2.85	3.85	7.97
LLDPE	20	16.6	1.59	3.30	4.46	9.24
LLDPE	20	11.7	1.27	2.88	3.56	8.08
LLDPE	20	15.2	1.27	2.59	3.55	7.25
HDPE	2	9.27	1.40	2.84	3.91	7.94
HDPE	2	9.63	1.23	2.75	3.45	7.71

13.2 Tables 7 through 10 are based on a round robin test conducted by the polyolefin subcommittee in 1988, involving eight polyethylene materials tested in ten laboratories. For each material, all samples were molded at one source, but the individual specimens were prepared at the laboratories that tested them. Each test result was the average of five individual determinations. Each laboratory obtained three test results for each material. Data from some laboratories could not be used for various reasons, and this is noted in each table.

**TABLE 9 Tensile Break Strength, for Nine Laboratories, Six Materials**

Material	Test Speed, in./min	Values Expressed in psi Units				
		Average	S <sub>r</sub>	S <sub>R</sub>	I <sub>r</sub>	I <sub>R</sub>
LDPE	20	1592	52.3	74.9	146.4	209.7
LDPE	20	1750	66.6	102.9	186.4	288.1
LLDPE	20	4379	127.1	219.0	355.8	613.3
LLDPE	20	2840	78.6	143.5	220.2	401.8
LLDPE	20	1679	34.3	47.0	95.96	131.6
LLDPE	20	2660	119.1	166.3	333.6	465.6

**TABLE 10 Tensile Break Elongation, for Nine Laboratories, Six Materials**

Material	Test Speed, in./min	Values Expressed in Percent Units				
		Average	S <sub>r</sub>	S <sub>R</sub>	I <sub>r</sub>	I <sub>R</sub>
LDPE	20	567	31.5	59.5	88.2	166.6
LDPE	20	569	61.5	89.2	172.3	249.7
LLDPE	20	890	25.7	113.8	71.9	318.7
LLDPE	20	64.4	6.68	11.7	18.7	32.6
LLDPE	20	803	25.7	104.4	71.9	292.5
LLDPE	20	782	41.6	96.7	116.6	270.8

13.3 In Tables 2 through 10, for the materials indicated, and for test results that derived from testing five specimens:

13.3.1 S<sub>r</sub> is the within-laboratory standard deviation of the average; I<sub>r</sub>=2.83 S<sub>r</sub>. (See 13.3.3 for application of I<sub>r</sub>)

13.3.2 S<sub>R</sub> is the between-laboratory standard deviation of the average; I<sub>R</sub>= 2.83 S<sub>R</sub>. (See 13.3.4 for application of I<sub>R</sub>)

13.3.3 Repeatability—In comparing two test results for the same material, obtained by the same operator using the same equipment on the same day, those test results should be judged not equivalent if they differ by more than the I<sub>r</sub> value for that material and condition.

13.3.4 Reproducibility—In comparing two test results for the same material, obtained by different days, those test results should be judged not equivalent if they differ by more than the I<sub>R</sub> value for that material and condition. (This applies between different laboratories or between different equipment within the same laboratory.)

13.3.5 Any judgment in accordance with 13.3.3 and 13.3.4 will have an approximate 95% (0.95) probability of being correct.

13.3.6 Other formulations may give somewhat different results.

13.4 For further information on the methodology used in this section, see Practice E 691.

- 13.5 There are no recognized standards on which to base an estimate of bias for this test method.
- 13.6 The precision of this test method is very dependent upon the uniformity of specimen preparation, standard practices for which are covered in other documents.

14. Keywords

- 14.1 Modulus of elasticity; percent elongation; plastics; tensile properties; tensile strength

**ANNEXES**

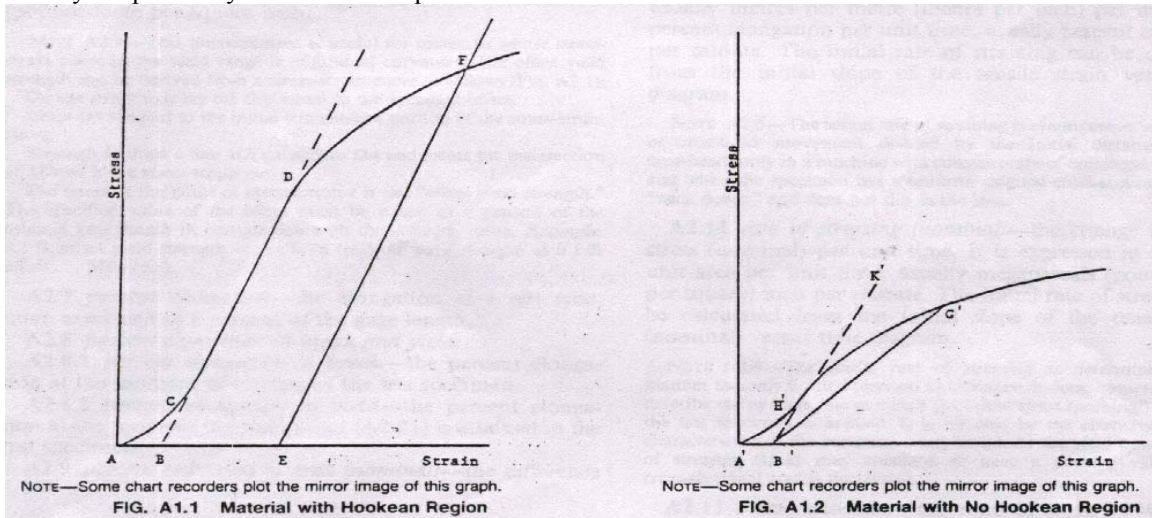
**(Mandatory Information)**

**A1. TOE COMPENSATION**

A1.1 In a typical stress-strain curve (Fig. A1.1) there is a toe region, AC, that does not represent a property of the material. It is an artifact caused by a takeup of slack, and alignment or seating of the specimen. In order to obtain correct values of such parameters as modulus, strain, and offset yield point, this artifact must be compensated for to give the corrected zero point on the strain or extension axis.

A1.2 In the case of a material exhibiting a region of Hookean (linear) behavior (Fig. A1.1), a continuation of the linear (CD) region of the curve is constructed through the zero-stress axis. This intersection (B) is the corrected zero-strain point from which all extensions or strains must be measured, including the yield offset (BE), if applicable. The elastic modulus can be determined by dividing the stress at any point along the line DC (or its extension) by the strain at the same point (measured from point B, defined as zero-strain).

A1.3 In the case of a material that does not exhibit any linear region (Fig. A1.2), the same kind of toe correction of the zero-strain point can be made by constructing a tangent to the maximum slope at the inflection point (H'). This is extended to intersect the strain axis at point B', the corrected zero-strain point. Using point B' as zero strain, the stress at any point (G') on the curve can be divided by the strain at that point to obtain a secant modulus (slope of line B' G'). For those materials with no linear region, any attempt to use the tangent through the inflection point as a basis for determination of an offset yield point may result in unacceptable error.



**A2. DEFINITIONS OF TERMS AND SYMBOLS RELATING TO TENSION TESTING OF PLASTICS**

A2.1 elastic limit—the greatest stress which a material is capable of sustaining without any permanent strain remaining upon complete release of the stress. It is expressed in force per unit area, usually pounds-force per square inch (megapascals).

NOTE A2.1—Measured values of proportional limit and elastic limit vary greatly with the sensitivity and accuracy of the testing equipment, eccentricity of loading, the scale to which the stress-strain diagram is plotted, and other factors. Consequently, these values are usually replaced by yield strength.

A2.2 elongation—the increase in length produced in the gage length of the test specimen by a tensile load. It is expressed in units of length, usually inches (millimeters). (Also known as extension.)

NOTE A2.2—Elongation and strain values are valid only cases where uniformity of specimen behavior within the gage length is present. In the case of materials exhibiting necking phenomena, such values are only of qualitative utility after attainment of yield point. This is due to inability to assure that necking will encompass the entire length between the gage marks prior to specimen

failure.

A2.3 gage length—the original length of that portion of the specimen over which strain or change in length is determined.

A2.4 modulus of elasticity—the ratio of stress (nominal) to corresponding strain below the proportional limit of a material. It is expressed in force per unit area, usually megapascals (pounds-force per square inch) (Also known as elastic modulus or Young's modulus).

Note A2.3—The stress-strain relations of many plastics do not conform to Hooke's law throughout the elastic range but deviate therefrom even at stresses well below the elastic limit. For such materials the slope of the tangent to the stress-strain curve at a low stress is usually taken as the modulus of elasticity. Since the existence of a true proportional limit in plastics is debatable, the propriety of applying the term "modulus of elasticity" to describe the stiffness or rigidity of a plastic has been seriously questioned. The exact stress-strain characteristics of plastic materials are very dependent on such factors as rate of stressing, temperature, previous specimen history, etc. however, such a value is useful if its arbitrary nature and dependence on time, temperature, and other factors are realized.

A2.5 necking—the localized reduction in cross-section which may occur in a material under tensile stress.

A2.6 offset yield strength—the stress at which the strain exceeds by a specified amount (the offset) an extension of the initial proportional portion of the stress-strain curve. It is expressed in force per unit area, usually megapascals (pounds-force per square inch).

Note A2.4—This measurement is useful for materials whose stress-strain curve in the yield range is of gradual curvature. The offset yield strength can be derived from a stress-strain curve as follows (Fig. A2.1):

On the strain axis lay off OM equal to the specified offset.

Draw OA tangent to the initial straight-line portion of the stress-strain curve.

Through M draw a line MN parallel to OA and locate the intersection of MN with the stress-strain curve.

The stress at the point of intersection r is the "offset yield strength." The specified value of the offset must be stated as a percent of the original gage length in conjunction with the strength value.

Example: 0.1% offset yield strength = ...MPa (psi), or yield strength at 0.1% offset ... MPa (psi).

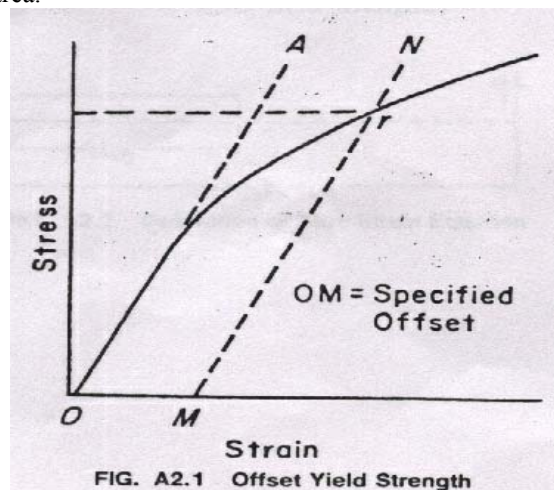
A2.7 percent elongation—the elongation of a test specimen expressed as a percent of the gage length.

A2.8 percent elongation at break and yield:

A2.8.1 percent elongation at break—the percent elongation at the moment of rupture of the test specimen.

A2.8.2 percent elongation at yield—the percent elongation at the moment the yield point (A2.21) is attained in the test specimen.

A2.9 percent reduction of area (nominal)—the difference between the original cross-sectional area measured at the point of rupture after breaking and after all retraction has ceased, expressed as a percent of the original area.



A2.10 percent reduction of area (true)—the difference between the original cross-sectional area of the test specimen and the minimum cross-sectional area within the gage boundaries prevailing at the moment of rupture, expressed as a percentage of the original area.

A2.11 proportional limit—the greatest stress which a material is capable of sustaining without any deviation from proportionality of stress to strain (Hooke's law). It is expressed in force per unit area,

usually megapascals (pounds-force per square inch).

A2.12 rate of loading—the change in tensile load carried by the specimen per unit time. It is expressed in force per unit time, usually newtons (pounds-force) per minute. The initial rate of loading can be calculated from the initial slope of the load versus time diagram.

A2.13 rate of straining—the change in tensile strain per unit time. It is expressed either as strain per unit time, usually metres per metre (inches per inch) per minute, or percent elongation per unit time, usually percent elongation per minute. The initial rate of straining can be calculated from the initial slope of the tensile strain versus time diagram.

Note A2.5—The initial rate of straining is synonymous with the rate of crosshead movement divided by the initial distance between crossheads only in a machine with constant-rate-crosshead movement and when the specimen has a uniform original cross-section, does not “neck down,” and does slip in the jaws.

A2.14 rate of stressing (nominal)—the change in tensile stress (nominal) per unit time. It is expressed in force per unit area per unit time, usually megapascals (pounds-force per square inch) per minute. The initial rate of stressing can be calculated from the initial slope of the tensile stress (nominal) versus time diagram.

Note A2.6—The initial rate of stressing as determined in this manner has only limited physical significance. It does, however, roughly describe the average rate at which the initial stress (nominal) carried by the test specimen is applied. It is affected by the elasticity and flow characteristics of the materials being tested. At the yield point, the rate of stressing (true) may continue to have a positive value if the cross-sectional area is decreasing.

A2.15 secant modulus—the ratio of stress (nominal) to corresponding strain at any specified point on the stress-strain curve. It is expressed in force per unit area, usually megapascals (pounds-force per square inch), and reported together with the specified stress or strain.

Note A2.7—This measurement is usually employed in place of modulus of elasticity in the case of materials whose stress-strain diagram does not demonstrate proportionality of stress to strain.

A2.16 strain—the ratio of the elongation to the gage length of the test specimen, that is, the change in length per unit of original length. It is expressed as a dimensionless ratio.

A2.17 tensile strength (nominal)—the maximum tensile stress (nominal) sustained by the specimen during a tension test. When the maximum stress occurs at the yield point (A2.21), it shall be designated tensile strength at yield. When the maximum stress occurs at break, it shall be designated tensile strength at break.

A2.18 tensile stress (nominal)—the tensile load per unit area of minimum original cross-section, within the gage boundaries, carried by the test specimen at any given moment. It is expressed in force per unit area, usually megapascals (pounds-force per square inch).

Note A2.8—The expression of tensile properties in terms of the minimum original cross-section is almost universally used in practice. In the case of materials exhibiting high extensibility, or necking, or both, (A2.15) nominal stress calculations may not be meaningful beyond the yield point (A2.21) due to the extensive reduction in cross-sectional area that ensues. Under some circumstances it may be desirable to express the tensile properties per unit of minimum prevailing cross-section. These properties are called true tensile properties (that is, true tensile stress, etc.).

A2.19 tensile stress-strain curve—a diagram in which values of tensile stress are plotted as ordinates against corresponding values of tensile strain as abscissas.

A2.20 true strain (see Fig. A2.2) is defined by the following equation for  $\epsilon_T$ :

$$\epsilon_T = \int_{L_0}^L dL / L = \ln L / L_0$$

where:

dL = the increment of elongation when the distance between the gage marks is L,

L<sub>0</sub> = the original distance between gage marks, and

L = the distance between gage marks at any time.

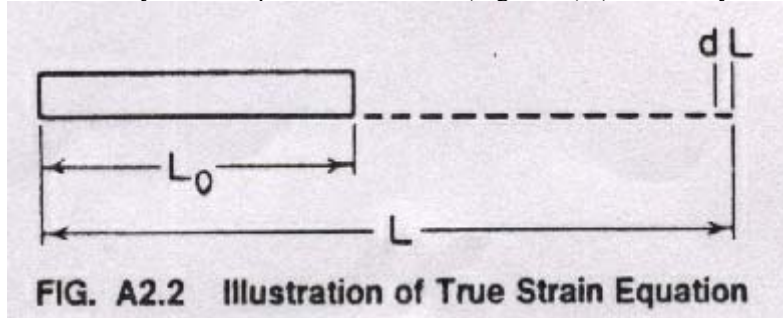
A2.21 yield point—the first point on the stress-strain curve at which an increase in strain occurs without an increase in stress (Fig. A2.2).

Note A2.9—Only materials whose stress-strain curves exhibit a point of zero slope may be considered as having a yield point.

Note A2.10—Some materials exhibit a distinct “break” or discontinuity in the stress-strain curve in the elastic region. This break is not a yield point by definition. However, this point may prove useful for material characterization in some cases.

A2.22 yield strength—the stress at which a material exhibits a specified limiting deviation from the proportionality of stress to strain. Unless otherwise specified, this stress will be the stress at the yield point and when expressed in relation to the tensile strength shall be designated either tensile strength

at yield or tensile stress as required under A2.17 (Fig. A2.3). (See offset yield strength.)



A2.23 Symbols—The following symbols may be used for the above terms:

SYMBOL	TERM
$W$	Load
$\Delta W$	Increment of load
$L$	Distance between gage marks at any time
$L_0$	Original distance between gage marks
$L_u$	Distance between gage marks at moment of rupture
$\Delta L$	Increment of distance between gage marks = elongation
$A$	Minimum cross-sectional area at any time
$A_0$	Original cross-sectional area
$\Delta A$	Increment of cross-sectional area
$A_u$	Cross-sectional area at point of rupture measured after breaking specimen
$A_T$	Cross-sectional area at point of rupture, measured at the moment of rupture
$T$	Time
$\Delta t$	Increment of time
$\sigma$	Tensile stress
$\Delta \sigma$	Increment of stress
$\sigma_T$	True tensile stress
$\sigma_U$	Tensile strength at break (nominal)
$\sigma_{UT}$	Tensile strength at break (true)
$\epsilon$	Strain
$\Delta \epsilon$	Increment of strain
$\epsilon_U$	Total strain, at break
$\epsilon_T$	True strain
$\%El$	Percentage elongation
$Y.P.$	Yield point
$E$	Modulus of elasticity

A2.24 Relations between these various terms may be defined as follows:

$$\begin{aligned} \sigma &= W/A_0 \\ \sigma_T &= W/A \\ \sigma_U &= W/A_0 \text{ (where } W \text{ is breaking load)} \\ \sigma_{UT} &= W/A_T \text{ (where } W \text{ is breaking load)} \\ \epsilon &= \Delta L/L_0 = (L-L_0)/L_0 \\ \epsilon_U &= (L_u-L_0)/L_0 \\ \epsilon_T &= \int_{L_0}^L dL/L = \ln L/L_0 \\ \%El &= [(L-L_0)/L_0] \times 100 = \epsilon \times 100 \end{aligned}$$

Percent reduction of area (nominal) =  $[(A_0 - A_u)/A_0] \times 100$

Percent reduction of area (true) =  $[(A_0 - A_T)/A_0] \times 100$

Rate of loading =  $\Delta W/\Delta t$

Rate of stressing (nominal) =  $\Delta \sigma/\Delta t = (\Delta W/A_0)/\Delta t$

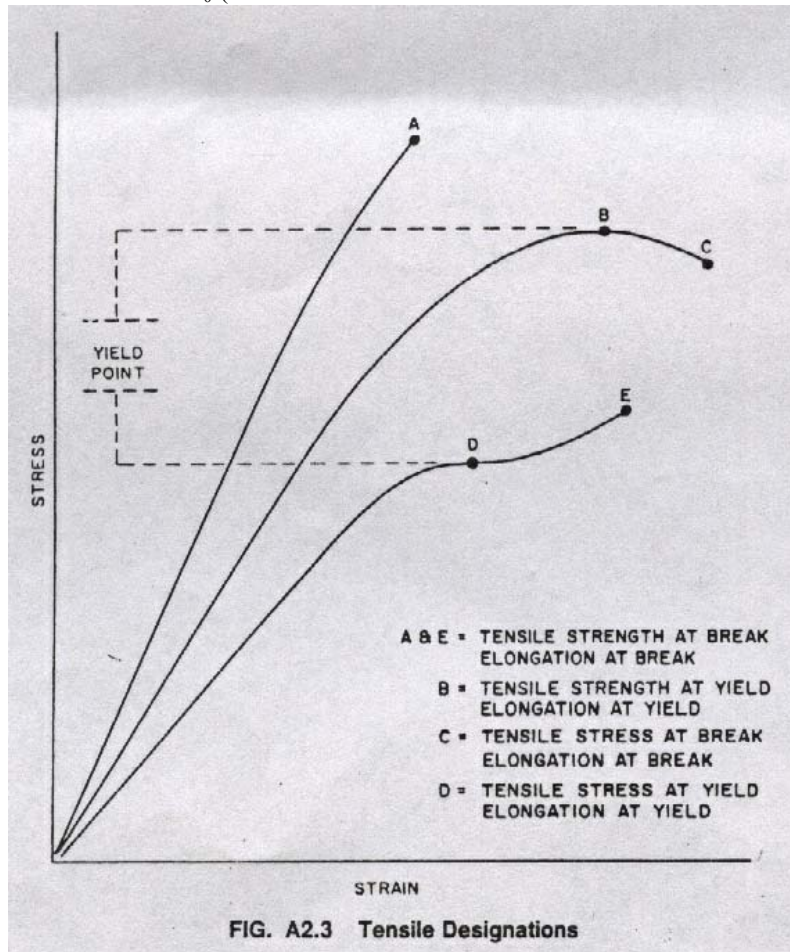
Rate of straining =  $\Delta \epsilon/\Delta t = (\Delta L/L_0)/\Delta t$

For the case where the volume of the test specimen does not change during the test, the following three relations hold:

$$\sigma_T = \sigma(1+\epsilon) = \sigma L/L_0$$

$$\sigma_{UT} = \sigma_v(1+\epsilon_v) = \sigma_v/L_{U1}/L_0$$

$$A = A_0/(1+\epsilon)$$



<sup>1</sup> This test methods are under the jurisdiction of ASTM Committee D-20 on Plastics and is the direct responsibility of Subcommittee D20.10 on Mechanical Properties. Current edition approved Oct. 15, 1994 and Dec. 15, 1994. Published February 1995. Originally published as D 638-41T. Last previous edition D 638-94. Section 5 was revised to allow for the use of fixed grips and an ISO equivalency statement was added since the last edition..

<sup>2</sup> Annual Book of ASTM Standards, Vol 10.01.

<sup>3</sup> Annual Book of ASTM Standards, Vol 09.01

<sup>4</sup> Annual Book of ASTM Standards, Vol 08.01.

<sup>5</sup> Annual Book of ASTM Standards, Vol 15.03.

<sup>6</sup> Annual Book of ASTM Standards, Vol 08.02.

<sup>7</sup> Annual Book of ASTM Standards, Vol 03.01.

<sup>8</sup> Annual Book of ASTM Standards, Vol 14.02.

<sup>9</sup> Available from American National Standard Institute, 11 W. 42<sup>nd</sup> St., 13<sup>th</sup> Floor, New York, NY 10036.

<sup>10</sup> Supporting data are available from ASTM Headquarters. Request RR: D20-1125 for the 1984 round and RR:D20-1170 for the 1988 round robin.